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### Discrete breathers in a mass-in-mass chain with Hertzian local resonators

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**Discrete breathers in a mass-in-mass chain with Hertzian local resonators**S. P. Wallen,<sup>1</sup> J. Lee,<sup>2</sup> D. Mei,<sup>2</sup> C. Chong,<sup>3</sup> P. G. Kevrekidis,<sup>2</sup> and N. Boechler<sup>1</sup><sup>1</sup>*Department of Mechanical Engineering, University of Washington, Seattle, Washington 98195, USA*<sup>2</sup>*Department of Mathematics and Statistics, University of Massachusetts, Amherst, Massachusetts 01003-4515, USA*<sup>3</sup>*Department of Mathematics, Bowdoin College, Brunswick, Maine 04011, USA*

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We report on the existence of discrete breathers in a one-dimensional, mass-in-mass chain with linear intersite coupling and nonlinear, precompressed Hertzian local resonators, which is motivated by recent studies of the dynamics of microspheres adhered to elastic substrates. After predicting theoretically the existence of discrete breathers in the continuum and anticontinuum limits of intersite coupling, we use numerical continuation to compute a family of breathers interpolating between the two regimes in a finite chain, where the displacement profiles of the breathers are localized around one lattice site. We then analyze the frequency-amplitude dependence of the breathers by performing numerical continuation on a linear eigenmode (vanishing amplitude) solution of the system near the upper band gap edge. Finally, we use direct numerical integration of the equations of motion to demonstrate the formation and evolution of the identified localized modes in energy-conserving and dissipative scenarios, including within settings that may be relevant to future experimental studies.

DOI: [10.1103/PhysRevE.95.022904](https://doi.org/10.1103/PhysRevE.95.022904)**I. INTRODUCTION**

Materials bearing local resonators are known to support unique dynamic phenomena, such as negative, highly anisotropic, and extreme effective properties [1,2]. Systems exhibiting these phenomena are commonly referred to as locally resonant metamaterials and are often described using linear dynamical models. One well-known model is a chain of mass-in-mass unit cells, which consists of a lattice of interconnected lumped masses, each with coupled local resonators [3]. By incorporating nonlinearity into locally resonant metamaterials, their dynamics become more complex. For example, metamaterials for both acoustic [2,4] and electromagnetic [4] waves have demonstrated numerous nonlinear phenomena, including tunability, harmonic generation, and the existence of nonlinear localized modes.

A promising means to create nonlinear acoustic metamaterials is provided by granular media, which consist of closely packed systems of particles that interact elastically. Granular media have been shown to support a wide range of nonlinear dynamic phenomena not encountered in conventional materials [5–8]. In granular materials, the microstructural geometric nonlinearity that stems from the shape of particles in contact (commonly modeled using Hertzian contact mechanics [9]) results in an effective macroscopic nonlinear material response. Previous works on granular media have demonstrated numerous nonlinear effects, including solitary waves, shocks, discrete breathers, tunable band gaps, frequency conversion, and nonreciprocal wave propagation [5–8].

Recent theoretical and experimental works have combined the concepts of locally resonant metamaterials with granular media. Relevant contexts include, but are not limited to, frequency shifting, harmonic generation, localized band-gap modes [10], traveling waves, including ones with nonvanishing tails [11,12], wave interaction [13], and other localized and extended modes [14], as well as temporally periodic breathing states [15,16] (to which we will return in what follows). In each of these examples, the granular media provided a nonlinear intersite coupling, while the local resonators were linear. Less

attention has been paid to cases in which granular particles play the role of nonlinear local resonators.

In this work, we consider a one-dimensional mass-in-mass system with linear intersite coupling and nonlinear local resonators that follow the Hertzian contact model with precompression. One motivation for considering this model is its relevance in describing a granular metamaterial consisting of a monolayer of microscale spheres adhered to a substrate, wherein surface localized elastic waves, such as Rayleigh surface acoustic waves (SAWs) and Lamb modes, have been shown to hybridize with the contact resonances of the microspheres in thick [17,18] and thin [19] substrates, respectively. Within this context, we imagine the portion of the substrate through which the localized elastic wave is traveling as a linearly coupled chain that is locally coupled to an array of nonlinear resonators representing the microspheres.

Systems similar to the one-dimensional, linearly coupled chain with nonlinear local resonators considered here have been previously explored. For example, amplitude-dependent band gaps have been studied in a one-dimensional linear chain with local resonators containing a cubic nonlinearity [20]. Other relevant works have also considered linear chains with nonlinear coupling to a rigid foundation [21], or a nonlinear local attachment [22], demonstrating heavily enriched dynamics caused by small nonlinear perturbations.

The structure of interest in the present work is the discrete breather (DB). Discrete breathers are solutions that are periodically oscillating in time and exponentially localized in space [23,24] that have been studied theoretically and experimentally in many settings, involving a wide array of physical mechanisms [25,26]. More recently, DBs have been demonstrated in theoretical [27,28] and experimental [29–31] studies of ordered granular chains without local resonators and theoretically in the presence of linear local resonators [15,16], as well as in nonlinear, locally resonant magnetic metamaterials [32–34] and systems of electromechanical resonators [35].

We use our model to describe a locally resonant granular metamaterial for Rayleigh SAWs, consisting of a monolayer

of microspheres adhered to a thick elastic substrate. The two independent model parameters are fit to an experimental system used in past work [17] so as to provide realistic parameter values to the model wherever possible. Beginning with the Hamiltonian version of our model, we predict the existence of DBs in the extreme limits of vanishing and strong intersite coupling, numerically compute a family of DBs connecting the two regimes, and examine the frequency-energy dependence of the DBs along the relevant branch of solutions. We then study the formation and evolution of the DBs via direct numerical simulations, considering both energy-conserving and dissipative cases, including within contexts that may be relevant to future experimental studies. While these results are presented in the context of a specific microscale system, we note that our model is given in dimensionless form such that the results presented herein can be applied and extended to related systems via a suitable choice of parameters (for example, one could create a model macroscale, locally resonant chain similar to the one studied in Ref. [10], but instead use linear springs to connect the main chain and Hertzian contacts in the internal resonators).

## II. MODEL

### A. Motivating physical scenario

Our chosen motivating physical scenario is shown in the schematic of Fig. 1(a), which describes sagittally polarized, plane SAWs traveling along the surface of a thick substrate. Rayleigh SAWs are surface localized elastic waves that travel along a solid surface (represented as an elastic half space in theoretical descriptions) and have both in- and out-of-plane (with respect to the sample surface plane) displacement components [36]. Previous studies on monolayers of microspheres adhered to thick substrates have shown that Rayleigh SAWs in the substrate hybridize with, and excite, microsphere contact resonances having translational out-of-plane [17] and coupled in-plane translational and rotational motion [18,37]. The hybridization with each of these resonances leads to classic avoided crossing phenomena [38] characteristic of locally resonant metamaterials and mass-in-mass chains. For the

analysis herein, we focus on the avoided crossing with the contact resonance having solely out-of-plane motion [17,18,37]. Because a plane SAW is confined to the surface of the medium, it can be considered as traveling in one dimension, and as such, we represent the portion of the substrate through which the SAW is traveling as an infinite lattice of lumped masses  $m_1$  connected by springs with linear stiffness  $k_1$ . Because the contact-based modes of the microspheres [17,18,39,40] have frequencies much lower than the intrinsic spheroidal vibrational frequencies of the isolated spheres [41] (e.g. for the microspheres studied in Ref. [17], the out-of-plane contact resonance was measured to be 215 MHz, while the spheroidal resonance was predicted to be 2.9 GHz), we model the microspheres as point masses (of mass  $m_2$ ) connected to the main chain by nonlinear springs modeling Hertzian contact with a static adhesive load. The resulting discrete model of our locally resonant granular metamaterial is shown in Fig. 1(b). As can be seen in Fig. 1(b), the chain elements are both drawn such that their motion is in the horizontal direction. We note that this depiction simply represents the coupling between a substrate (or chain) and a resonator, each having a single degree of freedom with the same, albeit arbitrary, direction of motion. Within the context of the previously described physical scenario, this degree of freedom represents out-of-plane motion of the substrate and the microsphere, as the SAWs propagate along the sample surface indexed by  $j$ .

### B. Hamiltonian 1D discrete model

In dimensionless form, the associated Hamiltonian equations of motion of the system shown in Fig. 1(b) read

$$M\ddot{u}_j + K(-u_{j+1} + 2u_j - u_{j-1}) + \frac{2}{3}([u_j - v_j + 1]_+^{3/2} - 1) = 0 \quad (1)$$

$$\ddot{v}_j - \frac{2}{3}([u_j - v_j + 1]_+^{3/2} - 1) = 0, \quad (2)$$

where  $u_j$  and  $v_j$  are, respectively, the displacements from equilibrium of the main chain and resonators,  $M = \frac{m_1}{m_2}$ ,  $K = \frac{k_1}{(3/2)A\sqrt{\delta_0}}$  characterizes the relative strength of the elastic and Hertzian terms, where the Hertzian coefficient  $A$  depends on the geometry and material properties of the particles in contact [9], and  $\delta_0$  is the static overlap induced by the adhesive force at equilibrium. The dimensionless time variable  $\tau$  is defined in terms of the physical time  $t$  by  $\tau = \frac{hs}{0}t$ , where  $\frac{hs}{0} = \sqrt{(3/2)A\sqrt{\delta_0}/m_2}$  is the resonant frequency of the local oscillator on the elastic half space (measured as 215 MHz for the system in Ref. [17]), and the displacements  $u_j$  and  $v_j$  are normalized to  $\delta_0$ . Here  $[\ ]_+$  indicates that the contact force vanishes for resonators that lose contact with the main chain, i.e., when the relative displacement  $v_j - u_j$  exceeds the static overlap. The Hamiltonian (energy) corresponding to Eqs. (1) and (2) is

$$H = \sum_j \left[ M \frac{\dot{u}_j^2}{2} + \frac{\dot{v}_j^2}{2} + \frac{K}{2} (u_{j+1}^2 - 2u_{j+1}u_j + u_j^2) + \frac{2}{3} \left( \frac{2}{5} [u_j - v_j + 1]_+^{5/2} - (u_j - v_j) \right) - \frac{4}{15} \right]. \quad (3)$$

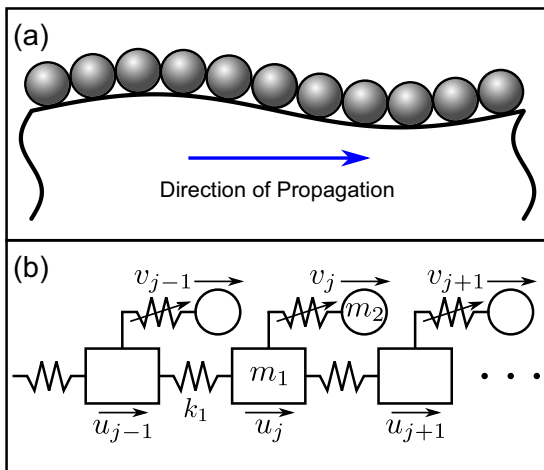


FIG. 1. (a) Granular metamaterial composed of a monolayer of microspheres on an elastic half space. (b) Schematic of the 1D, discrete granular metamaterial model.

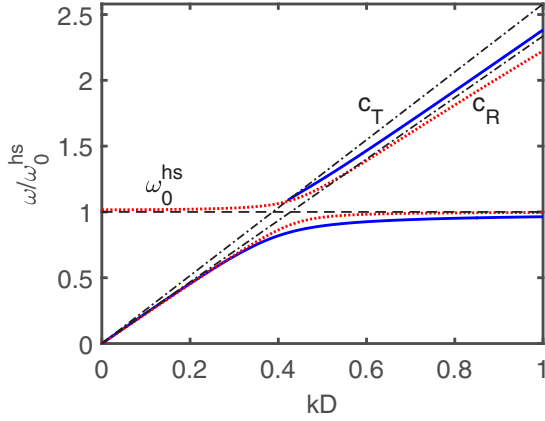


FIG. 2. Blue solid and red dotted curves denote the dispersion relations for the model with a continuous substrate from Ref. [17] and our discrete granular metamaterial model, respectively. Black dash-dotted lines have slopes equal to the transverse ( $c_T$ ) and Rayleigh ( $c_R$ ) wave sound speeds of the substrate. The black dashed line denotes the linear natural frequency of the Hertzian local resonators. The discrete model uses the fitted parameters  $M = 30$  and  $K = 160$ .

Upon linearization, this system is identical to the one-dimensional mass-in-mass chain discussed in [3]. Its dispersion relation is given by

$$M \left( \frac{\omega}{\omega_0^{\text{hs}}} \right)^4 - \{2K[1 - \cos(kD)] + M + 1\} \left( \frac{\omega}{\omega_0^{\text{hs}}} \right)^2 + 2K[1 - \cos(kD)] = 0, \quad (4)$$

where  $k$  is the Bloch wave number,  $\omega$  is the angular frequency, and  $D$  is the unit cell width, taken from the physical system as the width of the granular particles.

### C. Parameter fitting

The resulting model, as can be inferred from Eqs. (1) and (2), possesses two effective lumped parameters, namely,  $M$  and  $K$ . We now fit these discrete model parameters to describe the microgranular metamaterial of Ref. [17], using the material and geometric properties specified therein. We intend for the discrete model to provide an adequate representation of dynamical evolution for wavelengths significantly larger than the sphere diameter, such that the dispersion relations for our discrete model and the model with a continuous substrate from Ref. [17] are in close agreement at long wavelengths, and effects found at the Brillouin zone boundary [42] are avoided. The dispersion relations for a continuous substrate [from Eq. (2) of Ref. [17]] and the discrete model of Eqs. (1) and (2) are superimposed in Fig. 2. First, we choose the ratio  $K/M$  such that the long-wavelength sound speed of the discrete lattice, given by  $D\sqrt{K/M}$  [42], matches the speed of Rayleigh waves in the substrate for the model from Ref. [17]. This can be seen graphically in Fig. 2, as the lower branches of the two dispersion relations have equal slopes at the origin. Second, making use of the analytical expression for the dispersion relation of the continuous system in Ref. [17], we select  $K$  such that the dispersion relations coincide at the intersection with the line of slope  $c_T$ , where  $c_T$  is the transverse sound

speed of the substrate material. Using these two criteria, we find the approximate fitted values  $M = 30$  and  $K = 160$ .

The physical significance of these parameter values  $M$  and  $K$  is as follows. For large mass ratios ( $M \gg 1$ ), waves in the main chain (corresponding to Rayleigh SAWs in the substrate) are only perturbed at frequencies very close to the local resonance; this is confirmed in Fig. 2, by the relatively narrow band gap encompassing  $\omega/\omega_0^{\text{hs}} = 1$ . The large stiffness ratio ( $K \gg 1$ ) indicates strong coupling between lattice sites, compared to the coupling between the main chain and the resonators. Intuitively, parameters much greater than unity are indeed expected for this system. This is because the spheres are much smaller and less massive than the region of the substrate beneath them that is influenced by Rayleigh waves, whose displacements decay exponentially from the surface with a characteristic decay length on the order of one wavelength [36]. Similarly, the effective stiffness for the region of bulk material of the substrate influenced by the Rayleigh wave can be thought to have a significantly greater effective stiffness than the relatively soft microsphere-substrate Hertzian contact. While the fitted constants depend on material and geometric properties, a simple estimate can be used to show that  $M$  and  $K$  are generally larger than unity when considering long waves in realistic materials, as described in Appendices A and B.

Both of the dispersion relations shown in Fig. 2 are split, as a result of the hybridization with the local resonance, into two branches: the lower (acoustic) branch, in which the vertical motions of the substrate surface and the spheres are in phase, and the upper (optical) branch, in which the motions are out of phase. The two branches of the discrete model are separated by a band gap of width  $\Delta$ , given by

$$\Delta = \omega_0^{\text{hs}} \left( \sqrt{\frac{1+M}{M}} - \sqrt{\frac{4K+M+1 - \sqrt{(4K+M+1)^2 - 16KM}}{2M}} \right). \quad (5)$$

For the parameters values  $M$  and  $K$  used herein, this band gap results in an upper cutoff frequency of the acoustic branch 0.08% below  $\omega_0^{\text{hs}}$  and a lower cutoff frequency of the optical branch 1.65% above  $\omega_0^{\text{hs}}$ . In the continuous model, for phase velocities greater than the sound speed of transverse bulk waves ( $c_T$ ) in the substrate, the optical branch terminates; this is because the modes above that phase velocity are so-called leaky modes. Such leaky modes have complex frequency, which represents the radiation of energy into the bulk [17,43,44], and are a major source of dissipation in this system. Despite the presence of leaky modes, the one-dimensional discrete model used in this work was chosen over continuous and/or higher-dimensional models because it captures many of the important features of the dispersion relation (linear dispersion at long wavelengths and a band gap created by a local resonance), facilitates theoretical prediction and numerical computation of discrete breathers, and can easily be adapted to account for dissipation in a chosen experimental system (as will be demonstrated in Sec. V).

### III. THEORY

#### A. Anticontinuum limit

We start our analysis by considering the so-called anti-continuum (AC) limit of vanishing coupling. This approach, pioneered by MacKay and Aubry in [45], is based on the limit  $K \rightarrow 0$ , corresponding to uncoupled oscillators. While this limit is of limited physical relevance for our considerations herein, it is a particularly useful mathematical tool as a starting point for considering different breather-type configurations. This enables a natural starting point to seed continuation algorithms, which are then continued in the parameter  $K$  in order to identify solutions for different values of the relevant parameter. In the AC limit, our system has the form

$$M\ddot{u}_j = -\frac{2}{3}([u_j - v_j + 1]_+^{3/2} - 1), \quad (6)$$

$$\ddot{v}_j = \frac{2}{3}([u_j - v_j + 1]_+^{3/2} - 1). \quad (7)$$

We obtain a single oscillator by defining  $z = u_j - v_j$ , where

$$\ddot{z} = -\frac{2}{3}\tilde{\omega}_0^2([z + 1]_+^{3/2} - 1), \quad \tilde{\omega}_0^2 = \frac{1+M}{M}. \quad (8)$$

In addition to the trivial solution  $z = 0$ , there are nontrivial solutions of Eq. (8) that are the level curves of the energy  $E(z, \dot{z}) = \frac{1}{2}\dot{z}^2 + \frac{4(1+M)}{15M}([z + 1]_+^{5/2} - \frac{5}{2}z)$ . To construct a solution along the infinite lattice, each node is given as  $z = 0$  or the periodic function (say, with frequency  $\tilde{\omega}_b$ ) satisfying (8). In this paper, we consider the simplest such configuration, namely, the one consisting of zeros at every node with the exception of one [see Fig. 3(a)]. Due to Ref. [45] we know that this solution will persist for nonzero  $K$  as long as the so-called nonresonance condition  $\tilde{\omega}_b \neq n\tilde{\omega}_0^*$ ,  $n \in \mathbb{Z}$ , is satisfied, where  $\tilde{\omega}_0^* \in \{0, \tilde{\omega}_0\}$  is the frequency of solutions of the linearized equations at  $K = 0$ . While any such value of  $\tilde{\omega}_b$  will yield a persistent breather solution, we choose  $0 < \tilde{\omega}_b < \tilde{\omega}_0$ . Note that the two branches of the dispersion curves given by Eq. (4) bifurcate from 0 and  $\tilde{\omega}_0$  as the coupling  $K$  becomes nonzero. Thus, by choosing  $0 < \tilde{\omega}_b < \tilde{\omega}_0$  we are able to construct a band-gap breather. The numerical continuation (see Sec. IV) suggests that the solution constructed in the AC limit persists to the opposite limit  $K \rightarrow \infty$ . In this limit, other analytical techniques are available for the analysis of the solutions, which we explore next.

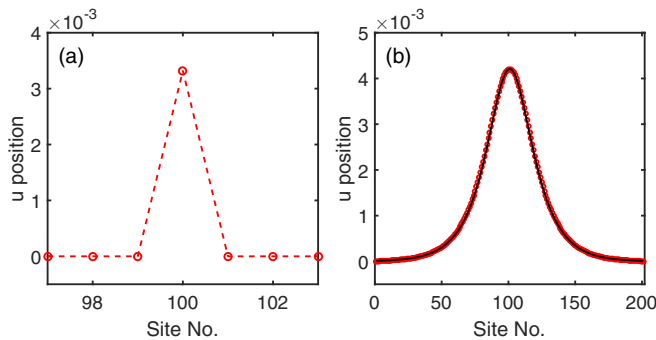


FIG. 3. (a) Single-site solution in the AC limit ( $K = 0$ ) with  $\tilde{\omega}_b = 1.01$ . (b) Breather profiles of frequency  $\tilde{\omega}_b = 1.01$  from the NLS ansatz (black solid curve) and numerical solution (red circle markers) with  $K = 160$ . Here we use  $M = 30$ .

#### B. Continuum limit and nonlinear Schrödinger approximation

For the purposes of the analysis, we consider small-amplitude solutions (i.e.,  $|u_j - v_j| \ll 1$ ). Thus, it is reasonable to expand the nonlinearity in a Taylor series

$$[1 + x]^{3/2} = 1 + \frac{3}{2}x + \frac{3}{8}x^2 - \frac{3}{48}x^3 + \dots,$$

where the dots denote higher-order terms. In addition, if we formally consider  $K = 1/D^2$ , where  $D$  is the lattice spacing and we let  $D \rightarrow 0$ , then Eqs. (1) and (2) become

$$M\partial_{\tau\tau}u - \partial_{xx}u + (u - v) + \frac{1}{4}(u - v)^2 - \frac{1}{24}(u - v)^3 = 0, \quad (9)$$

$$\partial_{\tau\tau}v - (u - v) - \frac{1}{4}(u - v)^2 + \frac{1}{24}(u - v)^3 = 0. \quad (10)$$

We approximate solutions of the above set of equations with the ansatz

$$u^{\text{an}} = \varepsilon A(X, T)E(x, \tau) + \text{c.c.} + \dots,$$

where  $X = \varepsilon(x - c\tau)$ ,  $T = \varepsilon^2\tau$ ,  $A = A(X, T)$ , and  $E = E(x, \tau) = e^{i(kx + \tilde{\omega}\tau)}$ , where  $k$  is the Bloch wave number,  $\tilde{\omega} = \tilde{\omega}_0 + \frac{\hbar\omega}{\hbar\omega_0}$ , and  $\varepsilon$  is some small positive parameter. Substitution of the ansatz into Eqs. (9) and (10) and equating the various orders of  $\varepsilon$  yields a hierarchy of solvability conditions. The particular choice of ansatz is well known to yield a nonlinear Schrödinger (NLS) equation for the envelope function  $A(X, T)$  in the theory of nonlinear waves [46]. For our system, in order to derive the NLS equation, we need several higher-order terms

$$u^{\text{an}} = \varepsilon AE + \varepsilon^2 a_2 A_1 E^2 + \varepsilon^3 a_4 A_3 E^3 + \varepsilon^3 a_6 A_5 + \varepsilon^3 a_8 A_7 E^2 + \varepsilon^3 a_{10} A_9 E + \text{c.c.}, \quad (11)$$

$$v^{\text{an}} = \varepsilon a_1 AE + \varepsilon^2 a_3 A_2 E^2 + \varepsilon^3 a_5 A_4 E^3 + \varepsilon^2 a_7 A_6 E + \varepsilon^3 a_9 A_8 E^2 + \varepsilon^3 a_{11} A_{10} E + \text{c.c.} + \varepsilon^2 a_{12} A \bar{A}, \quad (12)$$

where each  $A_i = A_i(X, T)$  and the  $a_i$  are real or complex coefficients. In particular, we will use

$$A_1 = A^2 = A_2, \quad A_3 = A^3 = A_4, \quad A_5 = \bar{A}\partial_X A, \\ A_6 = \partial_X A, \quad A_7 = A\partial_X A = A_8, \quad A_9 = \partial_T A, \quad A_{10} = \partial_X^2 A.$$

These relations are obtained through the solvability conditions, which can be found in Appendix C. We highlight here that at  $O(\varepsilon E)$  the solvability condition is the dispersion relation

$$M\tilde{\omega}^4 - [k^2 + M + 1]\tilde{\omega}^2 + k^2 = 0. \quad (13)$$

The connection between this dispersion relation and the one in Eq. (4) can be seen by Taylor expanding the cosine terms of Eq. (4). The NLS equation appears at  $O(\varepsilon^3 E)$ ,

$$[(M\tilde{\omega}^2 - k^2 - 1)a_{10} - 2iM\tilde{\omega}]\partial_T A \\ = (M\tilde{\omega}^2 - a_{11} - 1)\partial_X^2 A \\ + \left(\frac{1 - a_1}{2}(a_2 - a_3 - a_{12}) + \frac{(1 - a_1)^3}{8}\right)|A|^2 A. \quad (14)$$

Closed-form analytical solutions of the NLS equation (14) can be found via the inverse scattering transform [46]. One well known solution is the so-called bright soliton and is given by

$$A(X, T) = \sqrt{\gamma}\alpha \operatorname{sech}(\sqrt{\gamma}\beta X)e^{-i\gamma T}, \quad (15)$$



where  $\alpha$  and  $\beta$  are  $\epsilon$  independent coefficients that depend on the coefficients of the NLS equation (14) (see Appendix C) and  $\gamma > 0$  is an arbitrary parameter. Such solutions arise when the coefficient of the dispersion term and that of the nonlinearity have the same sign, which is the case for the parameter values chosen here.

Thus, at first order, we have the approximation

$$u(x, \tau) \approx \epsilon \sqrt{\gamma} \alpha \operatorname{sech}(\beta \sqrt{\gamma} X) e^{-i\gamma T} e^{i(kx + \tau)} + \text{c.c.}, \quad (16)$$

which is a traveling plane wave that is modulated by a small-amplitude, long-wavelength, and slowly varying localized function. For  $k = 0$ , this approximation reduces to

$$u(x, \tau) \approx \epsilon \sqrt{\gamma} \alpha \operatorname{sech}(\beta \epsilon \sqrt{\gamma} x) e^{i(\tilde{\omega}_0 - \gamma \epsilon^2) \tau} + \text{c.c.}, \quad (17)$$

which represents a standing breather with frequency  $\tilde{\omega}_b = \tilde{\omega}_0 - \gamma \epsilon^2$  [see Fig. 3(b)]. Here  $\tilde{\omega}_0^2 = (M + 1)/M$  represents the lower cutoff of the optical branch of the dispersion relation [see Eq. (4) with  $k = 0$ ]. Since  $\epsilon$  is a small parameter, the breather frequency  $\tilde{\omega}_b$  is near the lower cutoff of the optical branch, but within the gap. Note that the amplitude and width of the breather are both  $O(\epsilon \sqrt{\gamma})$ . Hence smaller-amplitude and wider breathers are found closer to the optical branch band edge. Recalling the results of the previous section on the AC limit, we were able to construct a breather solution with frequency  $\tilde{\omega}_b < \tilde{\omega}_0$ . If we define  $\gamma \epsilon^2 = \tilde{\omega}_0 - \tilde{\omega}_b$ , then our NLS approximation (17) (which is valid for large  $K$ ) will have, to first order, the same frequency as the AC limit breather (which is relevant for small  $K$ ). In the next section we will perform parametric continuation in  $K$  in order to connect the approximations in the two opposing limits  $K = 0$  and  $K \rightarrow \infty$ .

## IV. NUMERICAL INVESTIGATION OF BREATHERS

### A. Continuation in intersite coupling stiffness $K$

The analysis above allows us to describe breather solutions of Eqs. (1) and (2) in the limits  $K \rightarrow 0$  and  $K \rightarrow \infty$ . In order to connect these two pictures, we identify periodic orbits and explore their parametric continuation [47]. Our seed solution (initial guess) will be the AC limit solution with a single excited site [see Fig. 3(a)]. For the example considered in this section, we use the fitted value  $M = 30$  from Sec. II C and we choose the breather frequency  $\tilde{\omega}_b = 1.01$ . Note that in this case  $\tilde{\omega}_0 = \sqrt{1 + 1/30} > 1.01$ . For a fixed breather period  $T_b = 2\pi/\tilde{\omega}_b$ , we use the fact that  $u_j(0) = u_j(T_b)$  and  $v_j(0) = v_j(T_b)$  to construct the Poincaré map

$$P([u_0, v_0]; T_b) = \begin{bmatrix} \mathbf{u}(0; u_0, v_0) \\ \mathbf{v}(0; u_0, v_0) \end{bmatrix} - \begin{bmatrix} \mathbf{u}(T_b; u_0, v_0) \\ \mathbf{v}(T_b; u_0, v_0) \end{bmatrix}, \quad (18)$$

where  $\mathbf{u}(\tau; u_0, v_0) = \{u_n(\tau)\}_{n \in [0, N]}$  and  $\mathbf{v}(\tau; u_0, v_0) = \{v_n(\tau)\}_{n \in [0, N]}$  is the solution to Eqs. (1) and (2) with initial condition  $u(0) = u_0$  and  $v(0) = v_0$ . Therefore, a periodic solution with period  $T_b$  of Eqs. (1) and (2) will be a root to (18). A Newton-Raphson algorithm is used to approximate the roots of  $P$  [24]. The Jacobian is  $J = I - V(T_b)$ , where  $V(T_b)$  is the monodromy matrix. The eigenvalues of  $V(T_b)$  are the Floquet multipliers of the periodic solution. The breather is considered (spectrally) stable if all Floquet multipliers lie on

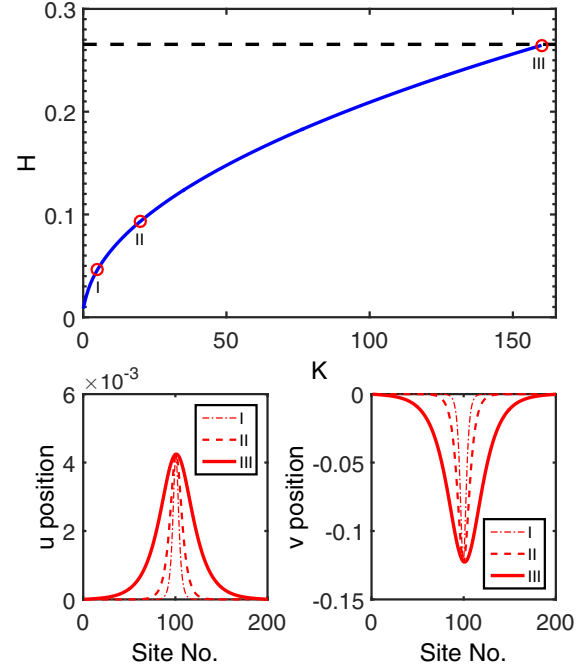


FIG. 4. The top panel is the continuation diagram (Hamiltonian energy versus coupling parameter  $K$ ), where the breather frequency and mass ratio are fixed as  $\tilde{\omega}_b = 1.01$  and  $M = 30$ , respectively. The dashed black line is the Hamiltonian of the NLS approximation of Eq. (17), given by Eq. (3), with  $K = 160$ . The bottom left and right panels are the main chain displacements  $u_j$  and the local resonator displacements  $v_j$ , respectively, taken at particular values of parameter  $K$ : for I,  $K = 5$ ; for II,  $K = 20$ ; and for III,  $K = 160$ .

the unit circle. Since the system is Hamiltonian, any Floquet multiplier lying off the unit circle signals instability [24].

The solution for a frequency ( $\tilde{\omega}_b = 1.01$ ) is found for  $K$  close to 0 (here  $K = 0.01$ ). Parameter continuation in  $K$  is performed and is plotted against the Hamiltonian energy of Eq. (3), as shown in Fig. 4. In this way, we are able to trace out a branch of solutions that emanates from the AC limit and approaches the continuum limit solution, which is well described by the NLS approximation of Eq. (17) (see the black dashed line of Fig. 4). Here we terminate the continuation at  $K = 160$ , which corresponds to the stiffness parameter extracted by fitting the discrete model to the locally resonant half-space model from Ref. [17] (see Sec. II C).

The numerical computations were performed on a system of 201 unit cells. This solution was spectrally stable for all values of  $K$  considered.

### B. Continuation in frequency $\tilde{\omega}$

The continuation in  $K$  of the previous section was terminated at the parameter value  $K = 160$  (note that  $M = 30$  and  $\tilde{\omega}_b = 1.01$ ). We now set  $M = 30$  and  $K = 160$  and vary the breather frequency  $\tilde{\omega}_b$  using a pseudo-arc-length continuation procedure [48,49]. This allows us to visualize the energy-frequency dependence of the breathers, as may be studied in an experiment with varied excitation amplitude.

As a seed for the continuation, we use the eigenmode of the linearized system nearest the lowest optical band edge, which

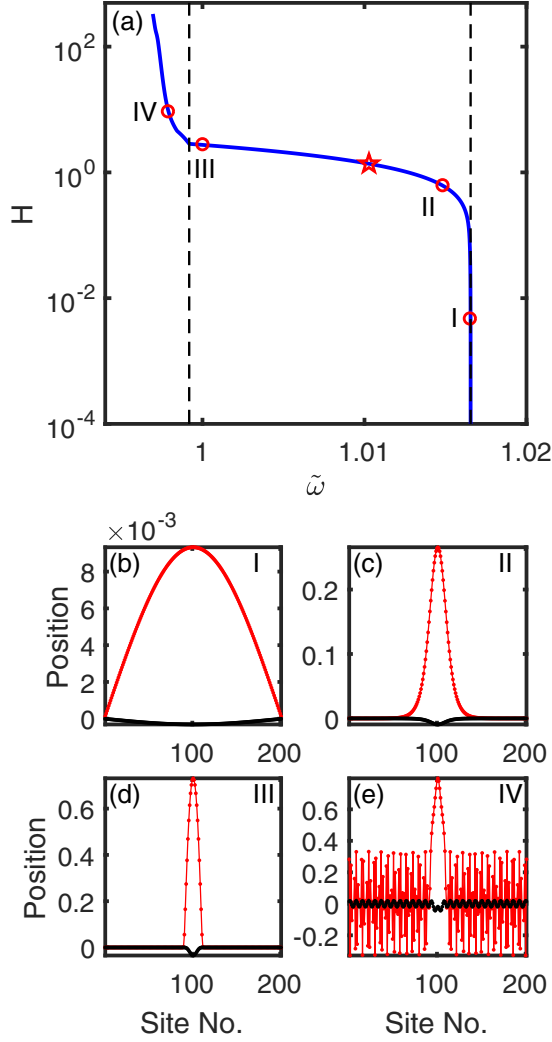


FIG. 5. (a) Hamiltonian energy-frequency plot of the family of breather solutions bifurcating from the lowest eigenmode of the optical band. Black dashed lines indicate the edges of the linear phonon band gap. The red star corresponds to the breather shown in Fig. 3(b). (b)–(e) Breather displacement profiles corresponding to the points labeled I–IV, respectively, in (a). The main chain displacements  $u_j$  are shown as black points and those of the local resonators  $v_j$  are shown in red.

is a time-periodic solution of the full nonlinear equations of motion under conditions of vanishing amplitude. We have included a check in our computations to detect a loss of contact between the main chain and resonators and continue the solution branch until this point.

As shown in Fig. 5, the continuation reveals a family of DBs that extends from the linear eigenmode at vanishing amplitude and traverses the band gap (and into the passband). In Fig. 6(a), we show the maximum magnitudes of the Floquet multipliers of the branch. This family of DBs exhibits behavior similar to those found in previous studies of diatomic granular chains [27], where the DBs are linearly stable for frequencies very close to the lower cutoff frequency of the optical branch. As the frequency decreases, the breather profiles become progressively more localized in space, as can be seen in

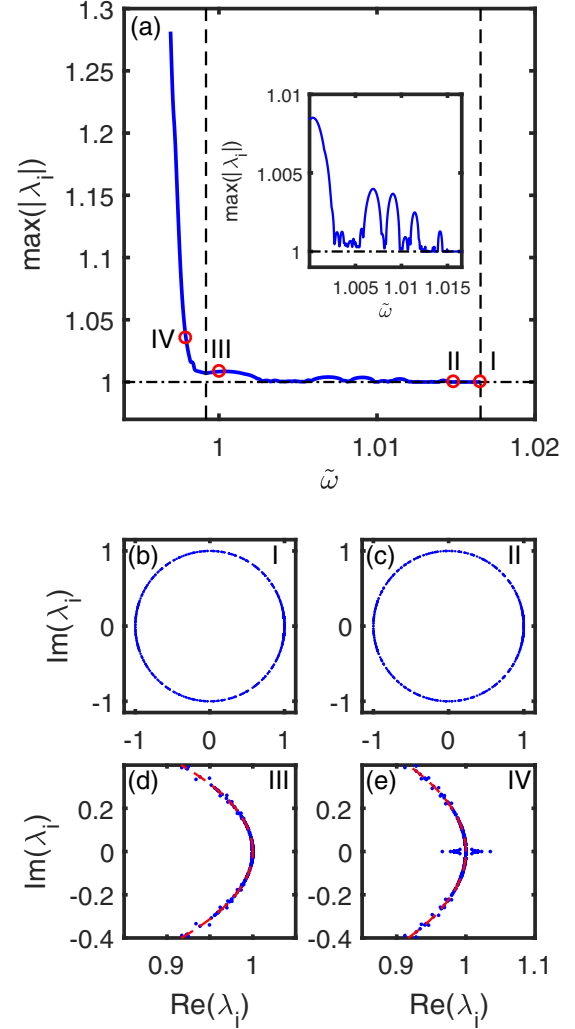


FIG. 6. (a) The blue solid curve shows the maximum magnitude of the breather Floquet multipliers. Black dashed lines indicate the edges of the linear phonon band gap and the inset shows a magnified view of the data in this range. (b)–(e) Floquet multipliers (blue dots) of the solutions labeled I–IV, respectively, in (a), corresponding to the same points in Fig. 5. In (d) and (e), axis limits are chosen to emphasize the deviation from the unit circle, which is shown as a visual aid (red dashed lines).

Figs. 5(b)–5(d). The Floquet multipliers corresponding to the modes shown in Figs. 5(b)–5(d) are shown in Figs. 6(b)–6(d), where small deviations from the unit circle can be seen in the latter figures. For breather frequencies below the band gap, interactions with the acoustic band generate oscillating tails, as shown in Fig. 5(e), and Floquet multipliers depart from the unit circle along the real axis, as shown in Fig. 6(e). We note that boundary effects are significant in the presence of oscillating tails, so the finite-length DBs do not accurately approximate the case of an infinite lattice. As an aside, we also point out that contrary to what is the case in the work of [27,29] for a granular crystal, here the dependence of the energy (Hamiltonian) on the frequency is monotonic, hence, in accordance with the recent criterion of [50], no instability arises from changes of monotonicity in this dependence.



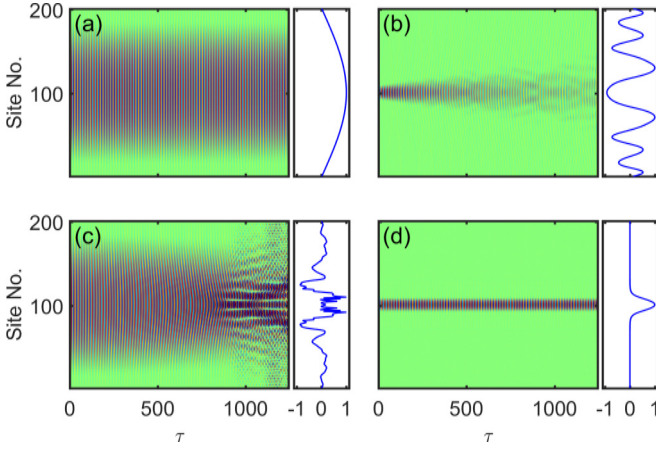


FIG. 7. Spatiotemporal plots of the relative displacements  $v_j - u_j$  of the simulated lattice for high- and low-amplitude excitations, using eigenmode and DB profiles as initial shapes. Side panels contain spatial profiles of  $v_j - u_j$  at the final time step, normalized to the maximum value. (a) Eigenmode shape with low amplitude (approximate periodic solution). (b) DB shape rescaled to low amplitude. (c) Eigenmode shape rescaled to high amplitude. (d) DB shape with high amplitude (exact periodic solution).

## V. NUMERICAL SIMULATIONS

### A. Hamiltonian case

To explore the dynamics of DBs in our model, we simulate a lattice with 201 unit cells via direct numerical integration of the equations of motion given by Eqs. (1) and (2). We consider initial conditions in two shapes: the profile of the DB with frequency  $\tilde{\omega}_b = 1.01$  and maximum Floquet multiplier magnitude  $\max(|\lambda_i|) = 1.001$  [as shown in Fig. 3(b) and denoted by the star in Fig. 5(a)], as well as the profile of the seeding eigenmode used in Sec. IV B.

For each of these shapes, we scale the amplitude in two ways. In the case of the DB shape, we consider the exact breather shape computed via continuation (high), and then consider a rescaled DB shape, such that the initial displacement  $v_{101}$  of the local resonator at the central lattice site is equal to one-hundredth of that of the exact solution (low). Similarly, we consider the shape of the seeding eigenmode, scaled such that the initial displacement  $v_{101}$  of the local resonator at the central lattice site is matched to the low-amplitude, rescaled DB shape (low), and then finally consider a rescaled eigenmode shape, such that the initial displacement  $v_{101}$  of the local resonator at the central lattice site is equal to that of the exact DB solution (high). Thus, there are four sets of initial conditions: the DB shape with high amplitude [Fig. 7(d)], which results in an exact periodic solution of Eqs. (1) and (2);

the eigenmode shape with low amplitude [Fig. 7(a)], which closely approximates a periodic solution; the DB shape rescaled to low amplitude [Fig. 7(b)], which is not a true periodic solution; and the eigenmode shape rescaled to high amplitude [Fig. 7(c)], which also is not a periodic solution. The duration of all simulations is  $200T_b$ , where  $T_b = 2\pi/\tilde{\omega}_b$  is the period of the exact DB solution.

Spatiotemporal plots of the relative displacements  $v_j - u_j$  of the simulated lattice, using the low- and high-amplitude DB profiles as initial conditions (i.e., the rescaled DB and exact solution), are shown in Figs. 7(b) and 7(d), respectively, and the corresponding cases using the eigenmode shape (i.e., the approximate periodic solution and corresponding rescaled profile) are shown in Figs. 7(a) and 7(c). As shown in Figs. 7(b) and 7(d), the breather shape spreads out from the central lattice sites at low amplitude, but remains highly localized when initiated with the energy of the exact solution. Conversely, as shown in Figs. 7(a) and 7(c), the eigenmode shape shows no noticeable distortion at low amplitude, but self-localizes and eventually breaks up at high amplitude. In this breakup, many smaller DBs are formed, a process arguably reminiscent of multiple filamentation in nonlinear optics [51], which also move in space. Thus, in future experiments on this system (e.g., using photoacoustic techniques, as in [17]), DBs could be detected by impulsively exciting a large spot on the substrate surface and observing the formation of smaller, highly localized wave packets.

### B. Effects of energy leakage

While we have considered a Hamiltonian model in this work as a foundation, energy losses may play an important role in the dynamics. The effects of losses have previously been examined in macroscopic granular systems [8,30,52–54] and also in the study of the attenuation of Rayleigh waves by randomly distributed surface resonators [44,55]. In this section, we conduct a preliminary study of energy losses on the DB dynamics, focusing on losses caused by radiation of energy into the bulk of the material, which is incurred by the long-wavelength leaky modes satisfying

$\omega > kc_T$  considered in previous sections. We first estimate the strength of dissipation by considering the rate of energy leakage into the substrate in the system studied in Ref. [17], in the long-wavelength limit. For a plane wave with real wave number  $k$  and complex frequency  $\omega + i\eta$ , the amplitude decays in time proportionally to  $e^{-\eta t}$ ; thus, the rate of decay is found by solving the dispersion relation for this complex frequency, with wave number  $k = 0$ . The dispersion relation (reproduced from Ref. [17] and substituting our own variable symbols) is given by

$$\left( \frac{2}{(\frac{hs}{0})^2} - 1 \left[ \left( 2 - \frac{2}{k^2 c_T^2} \right)^2 - 4 \left( 1 - \frac{2}{k^2 c_L^2} \right)^{1/2} \left( 1 - \frac{2}{k^2 c_T^2} \right)^{1/2} \right] \right) = \frac{m_2}{A_c \rho_1} \frac{4 \left( 1 - \frac{2}{k^2 c_L^2} \right)^{1/2}}{k^3 c_T^4}, \quad (19)$$

where  $m_2$  and  $\frac{hs}{0}$  are the mass and undamped natural frequency of the local resonator, respectively;  $A_c = \sqrt{3}/2D^2$

is the area of a unit cell containing a single microsphere of diameter  $D$ ;  $\rho_1$  is the density of the substrate; and  $c_L$  and

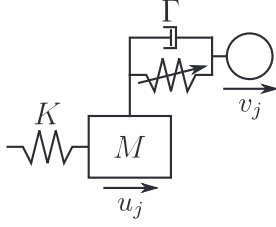


FIG. 8. Schematic of a single unit cell of the damped mass-in-mass lattice, with dimensionless parameters.

$c_T$  are the longitudinal and transverse bulk sound speeds of the substrate, respectively. We find a decay rate at  $k = 0$  of  $\eta_0 = m_2(\frac{hs}{0})^2/2A_c\rho_1c_L$ .

To facilitate comparison of the decay rate with other systems, we define the normalized decay rate  $\tilde{\eta} = 2\pi\eta/\omega$ , where  $1/\tilde{\eta}$  can be interpreted as the number of oscillation cycles needed to reduce the amplitude by a factor of  $e$  (at some characteristic frequency  $\omega$ ). For the material and geometric properties considered in this work, we estimate the normalized decay rate to be  $\tilde{\eta}_0 = 2\pi\eta_0/\omega^{hs} \approx 0.4$ .

Effects related to disorder, which have been discussed [17] and studied [44,55] in prior works on interactions between Rayleigh waves and surface oscillators, are also a potential major source of loss; however, in this study, we consider the possibility of highly ordered systems. In addition to radiative and disorder-related sources of loss, other types of dissipation will be present, but we expect them to be relatively small. For example, acoustic absorption in glass is about 0.5 dB/cm at frequencies near 200 MHz and room temperature [56]; assuming a Rayleigh wave with frequency  $\omega^{hs}$  and velocity of 3409 m/s [17], this results in  $\tilde{\eta} = 9 \times 10^{-5}$ . Aerodynamic drag in air (modeled by Stokes' Law, assuming 1  $\mu\text{m}$  diameter spheres [57]) results in  $\tilde{\eta} = 3 \times 10^{-4}$ . Finally, plastic deformation due to contact forces, if present, will not cause significant hysteresis during the elastic loading-unloading cycles.

To account for energy losses, in a way that is consistent with radiation into the bulk in the continuous granular metamaterial model, we modify our conservative system of equations (1) and (2) by placing a linear damper in each local resonator (as shown in Fig. 8) with a damping coefficient defined as  $\Gamma = \tilde{\eta}/\pi$  such that the exponential decay in time is proportional to  $e^{-\tilde{\eta}/(2\pi)\tau}$  and  $\Gamma_0 = \tilde{\eta}_0/\pi$ . With the damping included, the equations of motion become

$$M\ddot{u}_j + K(-u_{j+1} + 2u_j - u_{j-1}) + \frac{2}{3}([u_j - v_j + 1]_+^{3/2} - 1) + \Gamma(\dot{u}_j - \dot{v}_j) = 0, \quad (20)$$

$$\ddot{v}_j - \frac{2}{3}([u_j - v_j + 1]_+^{3/2} - 1) - \Gamma(\dot{u}_j - \dot{v}_j) = 0. \quad (21)$$

Using Eqs. (20) and (21), we repeat simulations of the 201-cell mass-in-mass chain, using the high-amplitude eigenmode and exact DB shapes [as in Figs. 7(c) and 7(d)] as initial conditions. The case  $\Gamma = \Gamma_0$  is shown in Figs. 9(a) and 9(b), where it can be seen that the oscillations die out after only a few oscillation cycles; this estimate indicates that the leakage of energy into the substrate may prohibit the observation of a standing localized mode in experiments on the particular system of

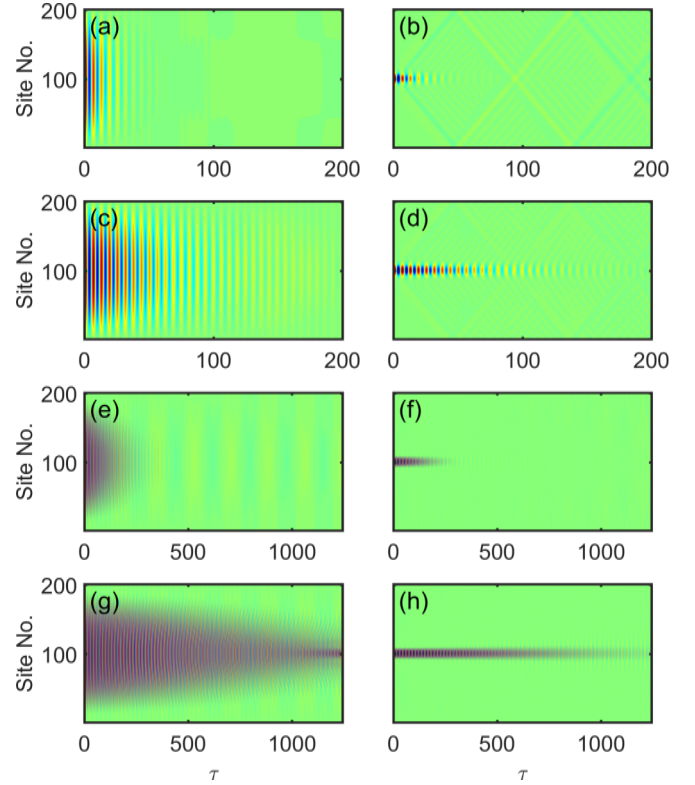


FIG. 9. Spatiotemporal plots of the relative displacements  $v_j - u_j$  of the simulated lattice for several damping coefficients: (a) and (b)  $\Gamma = \Gamma_0$ , (c) and (d)  $\Gamma = \Gamma_0/4$ , (e) and (f)  $\Gamma = \Gamma_0/16$ , and (g) and (h)  $\Gamma = \Gamma_0/100$ . Left and right panels correspond to the eigenmode (rescaled to high amplitude) and DB excitations used in Figs. 7(c) and 7(d).

Ref. [17], without adding further energy into the system to support the DB structure. However, this does not necessarily prohibit localized structures stemming from nonleaky modes. In this system, this corresponds to wave-number–frequency pairs below the line with slope  $c_T$  in Fig. 2. Such solutions would be traveling breathers and can be easily obtained from our analysis of Sec. III B by choosing a nonzero wave number in Eq. (16). A detailed investigation of such solutions would be a topic for future study.

In addition, while the attenuation due to energy leakage is significant for the monolayer of Ref. [17], it is straightforward to modify the system to reduce these losses by orders of magnitude; for example, if the spheres were instead placed with a spacing of  $10D$ , the unit cell area  $A_c$  would increase by a factor of 100, causing a proportional reduction in the damping coefficient  $\Gamma$ . As shown in Figs. 9(g) and 9(h), for the case  $\Gamma = \Gamma_0/100$ , the dynamics of the Hamiltonian model are retained for roughly half the simulation time (on the order of 100 oscillations) and localization around the central lattice site persists. Two intermediate cases are shown in Fig. 9(c) and 9(d) and Figs. 9(e) and 9(f), corresponding to damping coefficients  $\Gamma = \Gamma_0/4$  (sphere spacing  $2D$ ) and  $\Gamma = \Gamma_0/16$  (sphere spacing  $4D$ ), respectively. Very light damping could also be achieved in systems with different geometries, such as a thin substrate (e.g., the locally resonant membrane of Ref. [19]) without altering the unit cell spacing,

because energy would not be able to radiate. Additionally, we note that light damping (specifically, attenuation rates one order of magnitude smaller than Ref. [17]) has already been achieved experimentally in macroscale granular crystals. For example, both Refs. [52] and [30] characterized dissipation in experiments and found time constants on the order of a few milliseconds, at frequencies near 5 kHz, resulting in  $\tilde{\eta} \approx 0.08$  and  $\tilde{\eta} \approx 0.04$ , respectively, which suggests possible future realizations of our model at the macroscale.

## VI. CONCLUSION

In this work, we have demonstrated the existence of discrete breathers in a mass-in-mass chain that models a locally resonant, granular metamaterial composed of spheres adhered to a substrate. This model consists of a linearly coupled main chain (representing the substrate) with nonlinear local resonators that follow the Hertzian contact law (representing the spheres). After fitting the two independent model parameters to a microscale system studied in previous works, we analyzed the resulting energy trapping in the Hamiltonian version of our model, in the form of discrete breathers, theoretically, in the anticontinuum and continuum limits of intersite coupling, as well as numerically, by using the intersite coupling stiffness and oscillation frequency as continuation parameters. Finally, we simulated the formation and filamentation, in the form of discrete breathers, of single-humped wave packets using direct numerical integration of the equations of motion. The simulations suggest that discrete breathers may be observed in experiments on granular metamaterials by generating a long-wavelength excitation at high amplitude and detecting its breakup into many small discrete breathers. Simulations including energy losses suggest that the dynamics of the Hamiltonian model are mostly preserved in cases with light damping. However, in cases where the substrate is very thick, energy losses due to radiation into the bulk may inhibit the experimental observation of discrete breathers, though the leakage may be mitigated significantly by choosing suitable system parameters (e.g., the unit cell spacing, in the specific system discussed above). We expect this work to aid in future studies of nonlinear granular systems as well as the more general class of media composed of a linear material with local nonlinear resonant attachments. Indeed, the dynamics and interactions of discrete breathers (as well as their potential filamentation and dispersion) in one- to three-dimensional analogs of such systems may yield numerous topics that could be both theoretically intriguing and experimentally accessible for further study. Also, it should be borne in mind that here we only explored the focusing variants of the relevant models and their bright solitons. Yet, in line with recent explorations in granular crystals [30] and in systems with resonators [15], the self-defocusing case may also be interesting and equally accessible in different parametric regimes.

## ACKNOWLEDGMENTS

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## APPENDIX A: ESTIMATION OF THE MASS RATIO $M$

The local resonator mass is taken to be the mass of a single microsphere, given by  $m_2 = 4/3\pi(D/2)^3\rho_2$ , where  $\rho_2$  is the density of the microsphere material. We estimate the main chain mass as that of a rectangular region of the substrate beneath a single microsphere. Since Rayleigh SAWs have a characteristic decay length on the order of the wavelength  $\lambda$  [36], this region has mass  $m_1 = \lambda D^2\rho_1$ , where  $\rho_1$  is the density of the substrate material.

The mass ratio is then given by

$$M = m_1/m_2 = \left(\frac{6}{\pi}\frac{\rho_1}{\rho_2}\right)\frac{\lambda}{D}, \quad (\text{A1})$$

where the quantity in parentheses is expected to be of order  $\sim 1$  for most material combinations and the quantity  $\lambda/D$  is at least of order  $\sim 10^1$ , since we consider long wavelengths. Therefore, we estimate  $M \sim 10^1$ .

## APPENDIX B: ESTIMATION OF THE STIFFNESS RATIO $K$

The local resonator stiffness is taken from Hertzian contact theory [9], linearized about the static overlap distance  $\delta_0$  due to adhesion, using the same model as Ref. [17]. This stiffness is given by  $k_2 = (3/2)A\sqrt{\delta_0}$ . Here  $A = (4/3)E^*\sqrt{D/2}$ , with  $E^* = [(1 - \nu_1^2)/E_1 + (1 - \nu_2^2)/E_2]^{-1}$ , where  $E_{1,2}$  and  $\nu_{1,2}$  are Young's modulus and Poisson's ratio, respectively, with subscripts corresponding to the substrate and sphere materials [9]. The static overlap is  $\delta_0 = (F_{\text{DMT}}/A)^{2/3}$ , where  $F_{\text{DMT}} = \pi w D$  is the force due to adhesion as per the Derjaguin-Muller-Toporov adhesive elastic contact model [58] and  $w$  is the work of adhesion between the sphere and substrate materials. The main chain stiffness is estimated in a similar manner to the mass  $m_1$ , using an element of the substrate with length  $D$  in the direction of SAW propagation and cross-sectional area  $\lambda D$ . The estimated stiffness is then  $k_1 = E_1\lambda$ .

After algebraic manipulation, the stiffness ratio can be written as

$$K = k_1/k_2 \approx \left(\frac{8(1 - \nu_1^2)^2}{3\pi}\right)^{1/3} \left(\frac{E_1 D}{2w}\right)^{1/3} \frac{\lambda}{D}. \quad (\text{B1})$$

For simplicity, we have chosen to use identical sphere and substrate materials (so that  $E_2 = E_1$  and  $\nu_2 = \nu_1$ ); this approximation does not affect the generality of this rough estimate. The first term in parentheses is of order  $\sim 10^{-1}$  for realistic values of Poisson's ratio, i.e.,  $0 < \nu_1 < 0.5$ , and the second term in parentheses is of order  $\sim 10^2$ , for realistic values  $E_1 \sim 10^{10}$  and  $w \sim 10^{-2}$ , with  $D \sim 10^{-6}$ , using SI units. Since the quantity  $\lambda/D \sim 10^1$ , we estimate  $K \sim 10^2$ .

## APPENDIX C: DETAILS OF THE NLS DERIVATION

We define the residuals as

$$\text{res}(u) = -M\partial_{\tau\tau}u + \partial_{xx}u - (u - v) - \frac{1}{4}(u - v)^2 + \frac{1}{24}(u - v)^3, \quad (\text{C1})$$

$$\text{res}(v) = -\partial_{\tau\tau}v + (u - v) + \frac{1}{4}(u - v)^2 - \frac{1}{24}(u - v)^3. \quad (\text{C2})$$

Substituting  $u^{\text{an}}$  and  $v^{\text{an}}$  of Eqs. (11) and (12), we obtain the following residuals organized by orders of  $\varepsilon$ :

$$\begin{aligned} \text{res}(u^{\text{an}}) = & \varepsilon\{[\tilde{M} - k^2 - (1 - a_1)]AE\} + \varepsilon^2\{[(4\tilde{M} - 4k^2 - 1)a_2 + a_3 - \frac{1}{4}(1 - a_1)^2]A^2E^2 + (2ic\tilde{M} + 2ik + a_7)\partial_XAE \\ & + [a_{12} - \frac{1}{2}(1 - a_1)^2]A\bar{A}\} + \varepsilon^3\{(1 - Mc^2 + a_{11})\partial_X^2AE + [( \tilde{M} - k^2 - 1)a_{10} - 2i\tilde{M}] \partial_TAE + [\frac{1}{8}(1 - a_1)^3 \\ & - \frac{1}{2}(1 - a_1)(a_2 - a_3 - a_{12})]|A|^2AE + [8ic\tilde{M} + 8ika_2 + (4\tilde{M} - 4k^2 - 1)a_8 + a_9 + \frac{1}{2}(1 - a_1)a_7]A\partial_XAE^2 \\ & + [(9\tilde{M} - 9k^2 - 1)a_4 + a_5 - \frac{1}{2}(1 - a_1)(a_2 - a_3) + \frac{1}{24}(1 - a_1)^3]A^3E^3 + [\frac{1}{2}(1 - a_1)a_7 - a_6]\bar{A}\partial_XA\} + \text{c.c.} + \dots, \end{aligned} \quad (\text{C3})$$

$$\begin{aligned} \text{res}(v^{\text{an}}) = & \varepsilon\{[-\tilde{M} + (1 - a_1)]AE\} + \varepsilon^2\{[4\tilde{M} + (a_2 - a_3) + \frac{1}{4}(1 - a_1)^2]A^2E^2 + (2ic\tilde{M} + \tilde{M} - a_7 - a_7)\partial_XAE \\ & + [\frac{1}{2}(1 - a_1)^2 - a_{12}]A\bar{A}\} + \varepsilon^3\{(2ic\tilde{M} - c^2a_1 + \tilde{M} - a_{11})\partial_X^2AE + (a_{10} - 2i\tilde{M})\partial_TAE \\ & + [\frac{1}{2}(1 - a_1)(a_2 - a_3 - a_{12}) - \frac{1}{8}(1 - a_1)^3]|A|^2AE + [9\tilde{M} + (a_4 - a_5) + \frac{1}{2}(1 - a_1)(a_2 - a_3) - \frac{1}{24}(1 - a_1)^3]A^3E^3 \\ & + [8ic\tilde{M} + 4\tilde{M} + (a_8 - a_9) - \frac{1}{2}(1 - a_1)a_7]A\partial_XAE^2 + [a_6 - \frac{1}{2}(1 - a_1)a_7]\bar{A}\partial_XA\} + \text{c.c.} + \dots. \end{aligned} \quad (\text{C4})$$

If we set each order of  $\varepsilon$  to 0, we can define the coefficients  $a_i$  and parameters  $\tilde{M}$  and  $c$  such that  $\text{res}(u), \text{res}(v) = O(\varepsilon^4)$ , which should yield an accurate approximate solution to our original equations of motion. We now list the hierarchy of solvability conditions:  $O(\varepsilon AE)$ , the dispersion relation

$$M\tilde{M} - [1 + k^2 + M]\tilde{M} + k^2 = 0, \quad a_1 = 1 + k^2 - M\tilde{M};$$

$O(\varepsilon^2 A^2 E^2)$ ,

$$a_2 = -\frac{\tilde{M}(1 - a_1)^2}{1 + (1 - 4\tilde{M})(4\tilde{M} - 4k^2 - 1)},$$

$$a_3 = \frac{(a_1 - 1)^2 + 4a_2}{4 - 16\tilde{M}};$$

$O(\varepsilon^2 \partial_X AE)$ ,

$$a_7 = \frac{-2ika_1}{M(1 - \tilde{M}) + a_1}, \quad c = \frac{ia_7(\tilde{M} - 1)}{2\tilde{M}a_1};$$

$O(\varepsilon^2 A\bar{A})$ ,

$$a_{12} = \frac{1}{2}(1 - a_1)^2;$$

$O(\varepsilon^3 A^3 E^3)$ ,

$$a_4 = \frac{[12(1 - a_1)(a_2 - a_3) - (1 - a_1)^3]\tilde{M}}{24[k^2 - (1 + 9k^2 + M)\tilde{M} + 9M\tilde{M}]},$$

$$a_5 = \frac{24a_4 + 12(1 - a_1)(a_2 - a_3) - (1 - a_1)^3}{24(1 - 9\tilde{M})};$$

$O(\varepsilon^3 A\partial_X A E^2)$ ,

$$a_8 = \frac{8ia_2(k + c\tilde{M})(4\tilde{M} - 1) + 2a_7(1 - a_1)\tilde{M} - 8ic\tilde{M}a_3}{1 + (4\tilde{M} - 4k^2 - 1)(1 - 4\tilde{M})},$$

$$a_9 = \frac{16ic\tilde{M}a_3 + 2a_8 - (1 - a_1)a_7}{2 - 8\tilde{M}};$$

and  $O(\varepsilon^3 \bar{A}\partial_X A)$ ,

$$a_6 = \frac{1}{2}a_7(1 - a_1).$$

Finally, with these coefficients, we are left with two NLS equations at  $O(\varepsilon^3 E)$  of both  $\text{res}(u)$  and  $\text{res}(v)$ . In  $\text{res}(u)$ , we have

$$\begin{aligned} & [-2i\tilde{M} + (\tilde{M} - k^2 - 1)a_{10}]\partial_TA \\ & = -(1 - Mc^2 + a_{11})\partial_X^2A \\ & + \left(\frac{1 - a_1}{2}(a_2 - a_3 - a_{12}) - \frac{(1 - a_1)^3}{8}\right)|A|^2A \end{aligned} \quad (\text{C5})$$

and in  $\text{res}(v)$  we have

$$\begin{aligned} & -(-2i\tilde{M} + a_{10})\partial_TA \\ & = (2ic\tilde{M} + \tilde{M} - a_{11} - c^2a_1)\partial_X^2A \\ & + \left(\frac{(1 - a_1)^3}{8} - \frac{1 - a_1}{2}(a_2 - a_3 - a_{12})\right)|A|^2A. \end{aligned} \quad (\text{C6})$$

In order for both NLS equations to be satisfied, the coefficients in each must match. Thus, we require that

$$a_{10} = \frac{2i\tilde{M}(M + a_1)}{\tilde{M} - k^2}, \quad a_{11} = \frac{c^2(M + a_1) - 1 - 2ic\tilde{M}a_7}{\tilde{M}}$$

so that we obtain a single NLS equation. This equation has the solution

$$A(X, T) = \sqrt{\gamma}\alpha \text{sech}(\sqrt{\gamma}\beta X)e^{-i\gamma T},$$

with

$$\beta^2 = \frac{2\tilde{M} + (\tilde{M} - k^2 - 1)a_{10}i}{1 - Mc^2 + a_{11}}, \quad (\text{C7})$$

$$\alpha^2 = \frac{4\tilde{M} + 2(\tilde{M} - k^2 - 1)a_{10}i}{\frac{1}{8}(1 - a_1)^3 - \frac{1}{2}(1 - a_1)(a_2 - a_3 - a_{12})}, \quad (\text{C8})$$

and  $\gamma$  a free parameter.



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